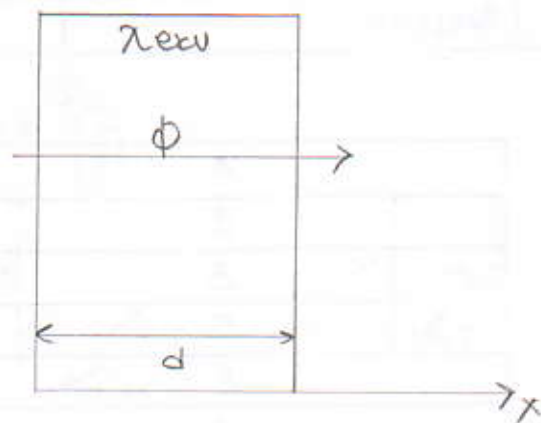
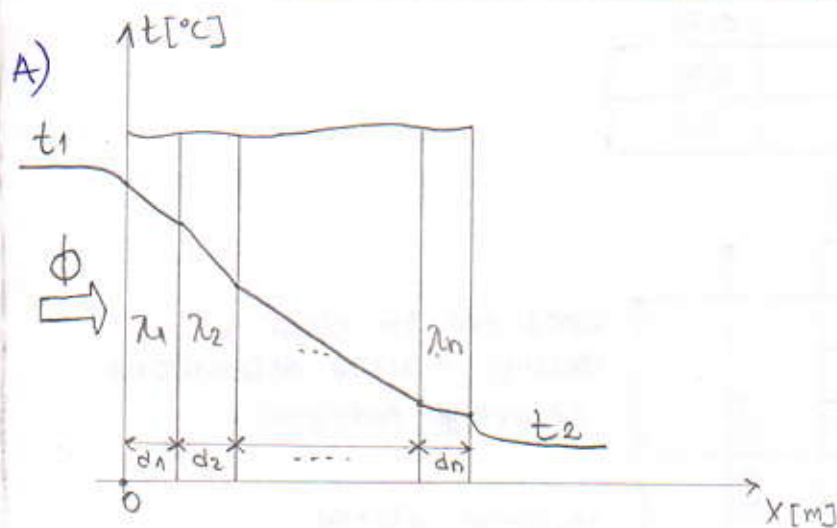


GRAĐEVINSKA FIZIKA - RAČUNSKE VEŽBE - II NEDELJA

1. A) Ravan nehomogen zid dimenzija $a \times b$ se sastoji od n slojeva debljina d_i , $i=1, \dots, n$. Zid je potrebno zameniti homogenim zidom iste debljine. Nađi ekvivalentnu toplotnu provodnost materijala homogenog zida tako da fluks toplotnih gubitaka nehomogenog i homogenog zida bude isti.

B) Ravan zid se sastoji od 4 sloja. Debljine i toplotne provodnosti slojeva su date u tabeli. Ako je spoljašnja temperatura vazduha 5°C , a unutrašnja 18°C , nađi toplotnu provodnost ekvivalentnog jednoslojnog zida tako da fluks toplotnih gubitaka jednoslojnog i višeslojnog zida bude isti.

Br.	Materijal	Debljina $d[\text{cm}]$	$\lambda[\frac{\text{W}}{\text{mK}}]$
1	Malter	1,5	1,4
2	Armirani beton	30	2,33
3	Staklena vuna	6	0,032
4	Produžni malter	1	0,99



$$\Phi_1 = \frac{t_1 - t_2}{\sum R_{Ti}} = \frac{t_1 - t_2}{\frac{1}{\alpha_1 s} + \sum_{i=1}^n \frac{d_i}{\lambda_i s} + \frac{1}{\alpha_2 s}} \quad [\text{W}]$$

$$\Phi_2 = \frac{t_1 - t_2}{R_{\text{rev}}} = \frac{t_1 - t_2}{\frac{1}{\alpha_1 s} + \frac{d}{\lambda_{\text{rev}} s} + \frac{1}{\alpha_2 s}}$$

$$d = d_1 + d_2 + \dots + d_n \quad \Phi_1 = \Phi_2$$

$$\frac{t_1 - t_2}{\frac{1}{\alpha_1 s} + \frac{1}{s} \sum_{i=1}^n \frac{d_i}{\lambda_i} + \frac{1}{\alpha_2 s}} = \frac{t_1 - t_2}{\frac{1}{\alpha_1 s} + \frac{d}{\lambda_{\text{rev}} s} + \frac{1}{\alpha_2 s}} \Rightarrow \sum_{i=1}^n \frac{d_i}{\lambda_i} = \frac{d}{\lambda_{\text{rev}}}$$

$$\boxed{\lambda_{\text{rev}} = \frac{d}{\sum_{i=1}^n \frac{d_i}{\lambda_i}} = \frac{\sum d_i}{\sum \frac{d_i}{\lambda_i}} = \frac{d}{\left(\frac{d_1}{\lambda_1} + \frac{d_2}{\lambda_2} + \dots + \frac{d_n}{\lambda_n}\right)}}$$

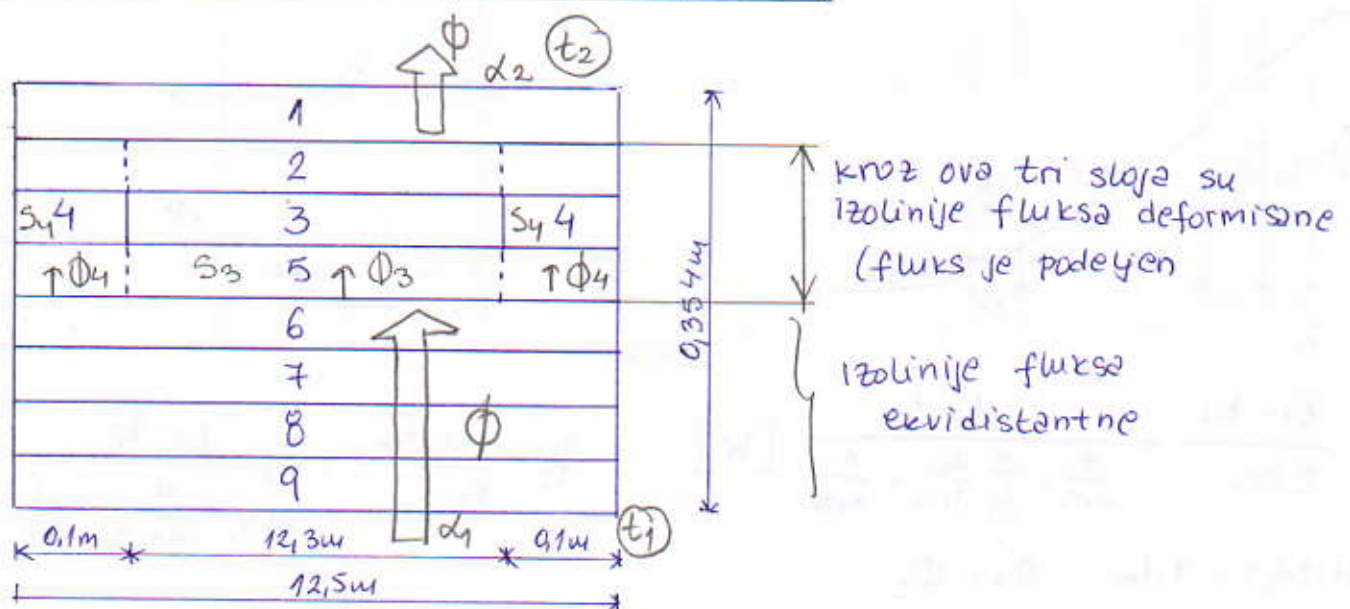
$$B) \lambda_{\text{rev}} = \frac{\sum_{i=1}^n d_i}{\sum_{i=1}^n \frac{d_i}{\lambda_i}} = \frac{d_1 + d_2 + d_3 + d_4}{\frac{d_1}{\lambda_1} + \frac{d_2}{\lambda_2} + \frac{d_3}{\lambda_3} + \frac{d_4}{\lambda_4}} = 0,190164 \frac{\text{W}}{\text{mK}}$$

② Izračunati termički otpor prolaza toplote, koeficijent prolaza toplote i R-vrednost za ravan višeslojni zid, dužine 30m i širine 12,5m čije su dimenzije i poprečni presek prikazani na slici. Zid je krov i deo je termičkog omotača zgrade. Koeficijenti prelaza toplote sa unutrašnje i spoljašnje strane zida su $10 \frac{\text{W}}{\text{m}^2\text{K}}$ i $25 \frac{\text{W}}{\text{m}^2\text{K}}$ respektivno. Toplotne provodnosti za pojedine materijale su date u tabeli. Prvi sloj u tabeli se nalazi sa spoljašnje strane zida, a poslednji sa unutrašnje.

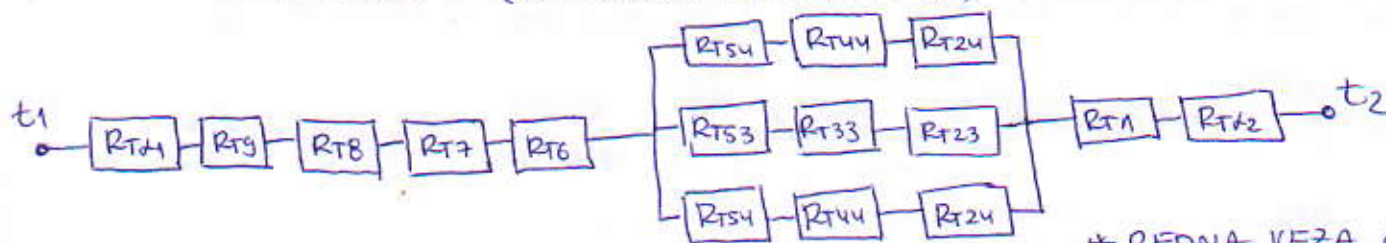
Br.	Materijal	Debljina d [cm]	$\lambda [\frac{\text{W}}{\text{mK}}]$
1	lepljena PVC membrana	0,5	0,19
2	Geotekstil	0,5	0,19
3	Durapor	12	0,035
4	Drvo-bor	12	0,14
5	Parna brana	0,4	0,19
6	Sloj za izravnavanje pritiska	2	0,81
7	Sloj za pad	2	0,76
8	AB ploča	16	2,33
9	Malter	2	1,4

$$\alpha_1 = 10 \frac{\text{W}}{\text{m}^2\text{K}}$$

$$\alpha_2 = 25 \frac{\text{W}}{\text{m}^2\text{K}}$$



→ ŠEMA OTPORNIKA (OBAVEZNO NACRTATI!)

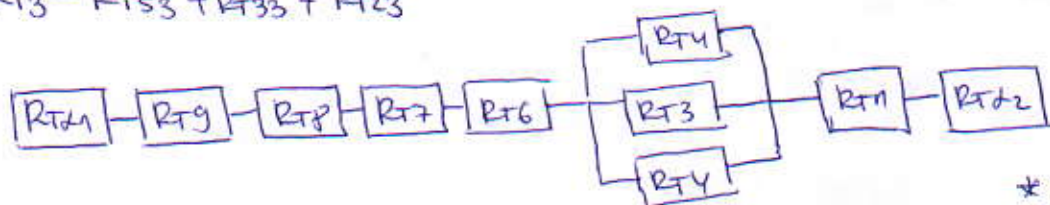


* REDNA VEZA OTPORNIKA:

$$R_{T4} = R_{T51} + R_{T53} + R_{T54}$$

$$R_{T3} = R_{T53} + R_{T33} + R_{T23}$$

$$R_{\text{ekv}} = \sum_i R_i$$



* PARALELNA VEZA OTPORNIKA:

$$\frac{1}{R_{T434}} = \frac{1}{R_{T4}} + \frac{1}{R_{T3}} + \frac{1}{R_{T4}} \Rightarrow R_{T434} = \frac{R_{T4} \cdot R_{T3}}{2R_{T3} + R_{T4}}$$

$$\frac{1}{R_{\text{ekv}}} = \sum_i \frac{1}{R_i}$$



$$R_T = R_{T1} + R_{T9} + R_{T8} + R_{T7} + R_{T6} + R_{T434} + R_{T11} + R_{T12}$$

→ ukupna površina zida:

$$S = 30 \cdot 12,5 = 375 \text{ m}^2$$

$$R_{T2i} = \frac{1}{\alpha_i \cdot S}$$

→ površina zida sa duroporom:

$$S_3 = 30 \cdot 12,3 = 369 \text{ m}^2$$

$$R_{Ti} = \frac{d_i}{\lambda_i \cdot S}$$

→ površina zida sa drvetom:

$$S_4 = 30 \cdot 0,1 = 3 \text{ m}^2$$

$$R_{Tij} = \frac{d_i}{\lambda_i \cdot S_j}$$

$$R_{T1} = \frac{1}{\alpha_1 \cdot S} = \frac{1}{10 \frac{\text{W}}{\text{m}^2 \cdot \text{K}} \cdot 375 \text{ m}^2} = 2,6 \cdot 10^{-4} \frac{\text{K}}{\text{W}}$$

$$R_{T2} = \frac{1}{\alpha_2 \cdot S} = \frac{1}{25 \frac{\text{W}}{\text{m}^2 \cdot \text{K}} \cdot 375 \text{ m}^2} = 1,06 \cdot 10^{-4} \frac{\text{K}}{\text{W}}$$

$$R_{T1} = \frac{d_1}{\lambda_1 \cdot S} = \frac{0,005 \text{ m}}{0,19 \frac{\text{W}}{\text{m} \cdot \text{K}} \cdot 375 \text{ m}^2} = 7,01754 \cdot 10^{-5} \frac{\text{K}}{\text{W}}$$

$$R_{T24} = \frac{d_2}{\lambda_2 \cdot S_4} = \frac{0,005}{0,19 \cdot 3} = 8,77193 \cdot 10^{-3} \frac{\text{K}}{\text{W}}$$

$$R_{T23} = \frac{d_2}{\lambda_2 \cdot S_3} = \frac{0,005}{0,19 \cdot 369} = 7,13165 \cdot 10^{-5} \frac{\text{K}}{\text{W}}$$

$$R_{T44} = \frac{d_4}{\lambda_4 S_4} = \frac{0,12}{0,14 \cdot 3} = 0,28571 \frac{K}{W}$$

$$R_{T33} = \frac{d_3}{\lambda_3 S_3} = \frac{0,12}{0,035 \cdot 369} = 9,29152 \cdot 10^{-3} \frac{K}{W}$$

$$R_{T54} = \frac{d_5}{\lambda_5 S_4} = \frac{0,004}{0,19 \cdot 3} = 7,01754 \cdot 10^{-3} \frac{K}{W}$$

$$R_{T53} = \frac{d_5}{\lambda_5 S_3} = \frac{0,004}{0,19 \cdot 369} = 5,70532 \cdot 10^{-5} \frac{K}{W}$$

$$R_{T6} = \frac{d_6}{\lambda_6 S} = \frac{0,02}{0,81 \cdot 375} = 6,58436 \cdot 10^{-5} \frac{K}{W}$$

$$R_{T7} = \frac{d_7}{\lambda_7 S} = \frac{0,02}{0,76 \cdot 375} = 7,01754 \cdot 10^{-5} \frac{K}{W}$$

$$R_{T8} = \frac{d_8}{\lambda_8 S} = \frac{0,16}{233 \cdot 375} = 1,83119 \cdot 10^{-4} \frac{K}{W}$$

$$R_{T9} = \frac{d_9}{\lambda_9 S} = \frac{0,02}{1,4 \cdot 375} = 3,80952 \cdot 10^{-5} \frac{K}{W}$$

$$R_{T4} = R_{T54} + R_{T24} + R_{T44} = 0,301504 \frac{K}{W}$$

$$R_{T3} = R_{T53} + R_{T23} + R_{T33} = 9,41989 \cdot 10^{-3} \frac{K}{W}$$

$$\left. \begin{array}{l} R_{T4} = 0,301504 \frac{K}{W} \\ R_{T3} = 9,41989 \cdot 10^{-3} \frac{K}{W} \end{array} \right\} R_{T434} = \frac{R_{T4} \cdot R_{T3}}{2R_{T3} + R_{T4}} = 8,865896 \cdot 10^{-3} \frac{K}{W}$$

$$R_T = R_{T41} + R_{T9} + R_{T8} + R_{T7} + R_{T6} + R_{T434} + R_{T1} + R_{T2} = 9,6666 \cdot 10^{-3} \frac{K}{W}$$

$$R\text{-vrednost } R = R_T \cdot S$$

$$R = (R_{T41} + R_{T9} + R_{T8} + R_{T7} + R_{T6} + R_{T1} + R_{T2}) \cdot S + R_{434}$$

$$R_{434} = \frac{R_4 \cdot R_3}{2R_3 + R_4}$$

$$R_4 = R_{T4} \cdot S_4 = 0,904511 \frac{K \cdot m^2}{W}$$

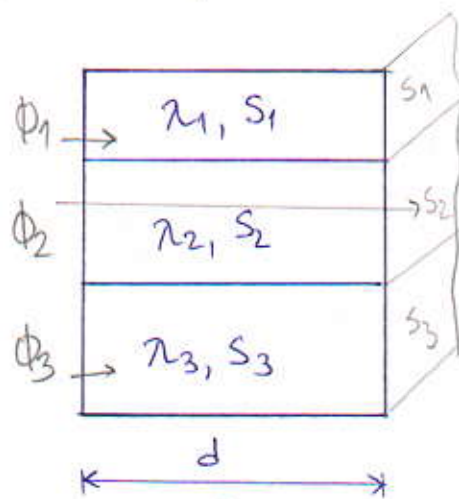
$$R_3 = R_{T3} \cdot S_3 = 3,475939 \frac{K \cdot m^2}{W}$$

$$R_{434} = 0,400187 \frac{K \cdot m^2}{W}$$

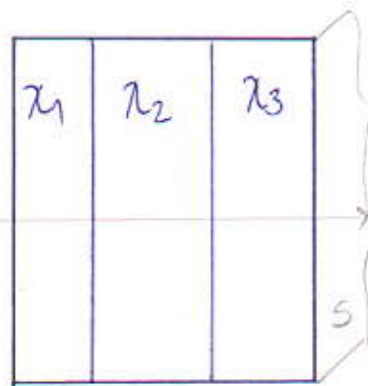
$$R = 8,00744 \cdot 10^{-4} \cdot 375 + 0,400187 = 0,70047 \frac{K \cdot m^2}{W}$$

$$U = \frac{1}{R} = \frac{1}{0,70047} = 1,42762 \frac{W}{K \cdot m^2}$$

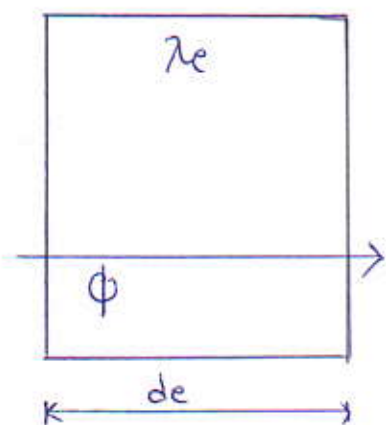
3. Ravan heterogen zid dužine L i visine H se sastoji od 3 sloja toplotnih provodnosti $\lambda_1, \lambda_2, \lambda_3$ i prikazan je na slikama a) i b) u poprečnom preseku. Naći ekvivalentne debljine de homogenih zidova za svaki od njih, ako je poznata toplotna provodnost λ_e , pod uslovom da su fluxevi toplotnih gubitaka zidova a) i b) i njima odgovarajućih homogenih zidova isti. Zanemariti prelaze toplote sa vazduha na zid i zid na vazduh.



a)



b)



a) $\phi = \phi_1 + \phi_2 + \phi_3$

$$\phi = \frac{\Delta t}{\frac{d}{\lambda_1 s_1}} + \frac{\Delta t}{\frac{d}{\lambda_2 s_2}} + \frac{\Delta t}{\frac{d}{\lambda_3 s_3}} = \frac{\Delta t}{\frac{d_e}{\lambda_e s}}$$

$$\frac{1}{\frac{d_e}{\lambda_e s}} = \frac{1}{\frac{d}{\lambda_1 s_1}} + \frac{1}{\frac{d}{\lambda_2 s_2}} + \frac{1}{\frac{d}{\lambda_3 s_3}}$$

$$\frac{\lambda_e \cdot s}{d_e} = \frac{\lambda_1 s_1 + \lambda_2 s_2 + \lambda_3 s_3}{d}$$

$$\Rightarrow d_e = \frac{\lambda_e \cdot d \cdot s}{\lambda_1 s_1 + \lambda_2 s_2 + \lambda_3 s_3}$$

$$d_e = \lambda_e \cdot \frac{(s_1 + s_2 + s_3) \cdot d}{\lambda_1 s_1 + \lambda_2 s_2 + \lambda_3 s_3}$$

$$* \frac{\lambda_1 s_1 + \lambda_2 s_2 + \lambda_3 s_3}{s_1 + s_2 + s_3} = \lambda_{sr}$$

b) $\phi = \frac{\Delta t}{\left(\frac{d_1}{\lambda_1} + \frac{d_2}{\lambda_2} + \frac{d_3}{\lambda_3}\right) \frac{1}{s}} = \frac{\Delta t}{\frac{d_e}{\lambda_e s}}$

$$\frac{\lambda_e}{d_e} = \frac{1}{\frac{d_1}{\lambda_1} + \frac{d_2}{\lambda_2} + \frac{d_3}{\lambda_3}} \Rightarrow$$

$$d_e = \lambda_e \left(\frac{d_1}{\lambda_1} + \frac{d_2}{\lambda_2} + \frac{d_3}{\lambda_3} \right)$$