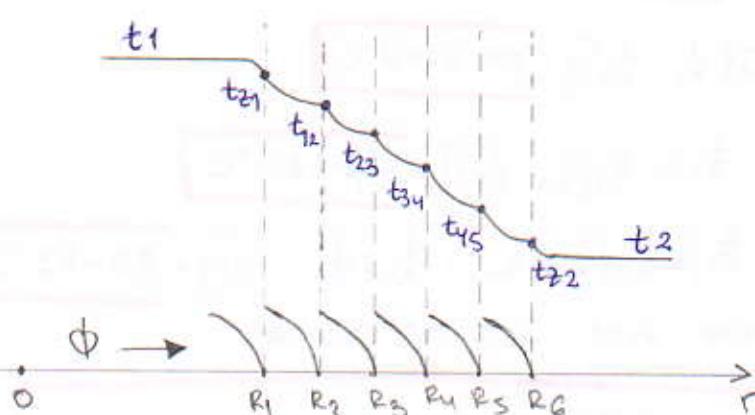


- ① Sferni zid, koji je deo termičkog omotača zgrade, sastoji se od pet slojeva. Unutrašnji poluprečnik posmatrane strukture je 3,2m. Debljine i toplotne provodnosti pojedinih slojeva su date u donjoj tabeli. Prvi sloj u tabeli se nalazi sa unutrašnje strane zida, a poslednji sa spoljašnje. Koeficijenti prelaza toplote sa unutrašnje i spoljašnje strane zida su $7,69 \frac{W}{m^2 \cdot K}$. Spoljašnja temperatura je $3^\circ C$, a temperatura unutar prostorije je $26^\circ C$. Ako su termalni kontakti između slojeva idealni, odrediti:
- Toplotni fluks
 - Ukupnu termalnu otpornost prolaza toplote posmatranog zida
 - Temperaturu zida sa spoljašnje i unutrašnje strane
 - Temperature na spojevima materijala
 - Temperatursko polje unutar kamene vune i giter bloka

Br.	Materijal	Debljina d [cm]	$\lambda \left[\frac{W}{m \cdot K} \right]$
1	Gips	2	0,15
2	Malter (unutra)	3	1,40
3	Giter blok	30	0,61
4	Kamena vuna	8	0,034
5	Malter (spolja)	2	1,40

$$t_1 = 26^\circ C \quad t_2 = 3^\circ C$$

$$\lambda_1 = 7,69 \frac{W}{m^2 \cdot K} \quad \lambda_2 = 7,69 \frac{W}{m^2 \cdot K}$$



$$R_1 = 3,2 m$$

$$R_2 = R_1 + d_1 = 3,2 + 0,02 = 3,22 m$$

$$R_3 = R_2 + d_2 = 3,25 m$$

$$R_4 = R_3 + d_3 = 3,55 m$$

$$R_5 = R_4 + d_4 = 3,63 m$$

$$R_6 = R_5 + d_5 = 3,65 m$$

a) Toplotni fluks

$$\Phi = \frac{t_1 - t_2}{R_T} = \frac{t_1 - t_2}{\frac{1}{2\pi} \left[\frac{1}{\lambda_1 R_1^2} + \sum_{i=1}^5 \frac{1}{\lambda_i} \left(\frac{1}{R_i} - \frac{1}{R_{i+1}} \right) + \frac{1}{\lambda_2 R_6^2} \right]}$$

$$\Phi = \frac{26-3}{\frac{1}{2\pi} \left[\frac{1}{7,69 \cdot (3,2)^2} + \frac{1}{0,5} \left(\frac{1}{3,2} - \frac{1}{3,22} \right) + \frac{1}{1,4} \left(\frac{1}{3,22} - \frac{1}{3,25} \right) + \frac{1}{0,61} \left(\frac{1}{3,25} - \frac{1}{3,55} \right) + \frac{1}{0,034} \left(\frac{1}{3,55} - \frac{1}{3,63} \right) + \frac{1}{1,4} \left(\frac{1}{3,63} - \frac{1}{3,65} \right) + \frac{1}{7,69 \cdot (3,65)^2} \right]} = 26-3$$

$$\Phi = \frac{23}{9040503420829} = 567,42196 \text{ W}$$

b) Termalna otpornost prolaza toplote

$$\Phi = \frac{\Delta t}{R_T} \Rightarrow R_T = \Phi \cdot \Delta t \quad R_T = 90405 \frac{\text{K}}{\text{W}}$$

c) Temperature zida sa spoljašnje i unutrašnje strane

$$t_{21} = t_1 - \frac{\Phi}{2\pi \lambda_1 R_1^2} = 24,853^\circ\text{C}$$

$$t_{22} = t_2 + \frac{\Phi}{2\pi \lambda_2 R_6^2} = 3,8815^\circ\text{C}$$

d) Temperature na spojevima materijala

$$t_{12} = t_1 - \frac{\Phi}{2\pi} \left[\frac{1}{\lambda_1 R_1^2} + \frac{1}{\lambda_1} \left(\frac{1}{R_1} - \frac{1}{R_2} \right) \right] = 24,5026^\circ\text{C}$$

$$t_{23} = t_1 - \frac{\Phi}{2\pi} \left[\frac{1}{\lambda_1 R_1^2} + \frac{1}{\lambda_1} \left(\frac{1}{R_1} - \frac{1}{R_2} \right) + \frac{1}{\lambda_2} \left(\frac{1}{R_2} - \frac{1}{R_3} \right) \right] = 24,3177^\circ\text{C}$$

$$t_{34} = t_1 - \frac{\Phi}{2\pi} \left[\frac{1}{\lambda_1 R_1^2} + \frac{1}{\lambda_1} \left(\frac{1}{R_1} - \frac{1}{R_2} \right) + \frac{1}{\lambda_2} \left(\frac{1}{R_2} - \frac{1}{R_3} \right) + \frac{1}{\lambda_3} \left(\frac{1}{R_3} - \frac{1}{R_4} \right) \right] = 20,4682^\circ\text{C}$$

$$t_{45} = t_1 - \frac{\Phi}{2\pi} \left[\frac{1}{\lambda_1 R_1^2} + \frac{1}{\lambda_1} \left(\frac{1}{R_1} - \frac{1}{R_2} \right) + \frac{1}{\lambda_2} \left(\frac{1}{R_2} - \frac{1}{R_3} \right) + \frac{1}{\lambda_3} \left(\frac{1}{R_3} - \frac{1}{R_4} \right) + \frac{1}{\lambda_4} \left(\frac{1}{R_4} - \frac{1}{R_5} \right) \right] = 3,9788^\circ\text{C}$$

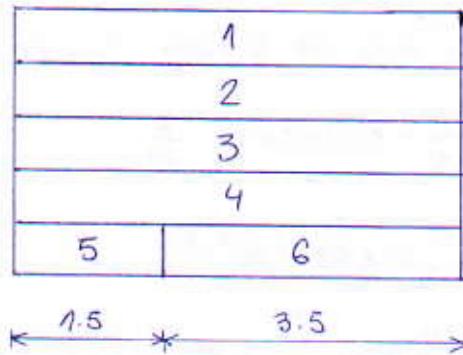
e) Temperatursko polje unutar kamenе vune i giter bloka

$$t_3(r) = t_{23} - \frac{\Phi}{2\pi} \cdot \frac{1}{\lambda_3} \left(\frac{1}{R_3} - \frac{1}{r} \right) = 24,3177[\text{ }^\circ\text{C}] - 148,045[\text{ }^\circ\text{C}\cdot\text{m}] \left(0,30769 - \frac{1}{r} \right)$$

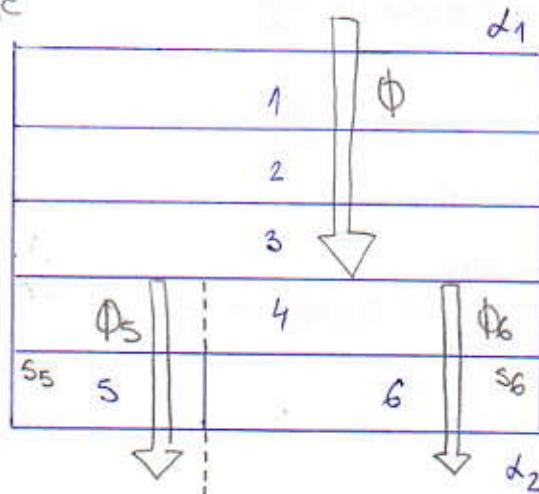
$$t_4(r) = t_{34} - \frac{\Phi}{2\pi} \frac{1}{\lambda_4} \left(\frac{1}{R_4} - \frac{1}{r} \right) = 20,4682[\text{ }^\circ\text{C}] - 2656,1118[\text{ }^\circ\text{C}\cdot\text{m}] \left(0,28169 - \frac{1}{r} \right)$$

2. Izračunati ekvivalentni termički otpor prolaza topline za ravan višeslojni zid i R-vrednost zida dužine 5m i širine 2,7m, čije su dimenzije i poprečni presek prikazani na slici. Zid je horizontalna međuspratna konstrukcija negrenjeg garaži i deo je termičkog omotača zgrade. Koeficijenti prolaza topline sa spoljašnje i unutrašnje strane zida su jednaki i iznose $s_{pp} \frac{W}{m^2 \cdot K}$. Koeficijenti topotne provodnosti za pojedine materijale su dati u tabeli. Prvi sloj u tabeli se nalazi sa gornje, a poslednji sa donje strane konstrukcije.

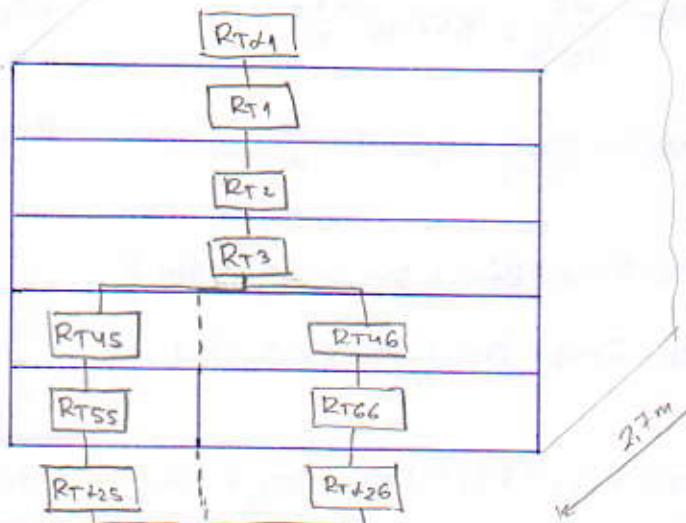
Br.	Materijal	Deklinina d [cm]	$\lambda \left[\frac{W}{m \cdot K} \right]$
1	Keramičke pločice	1	1,28
2	Cementni estrih	3	1,40
3	Gitter blok	10	0,61
4	Stirodur	3	0,035
5	Malter	2	1,40
6	Gips	2	0,70



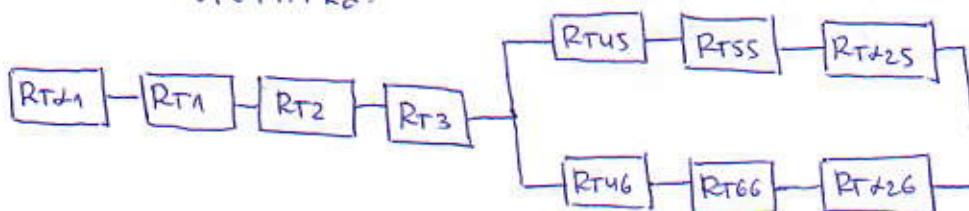
Prizemlje



Negrenja garaža

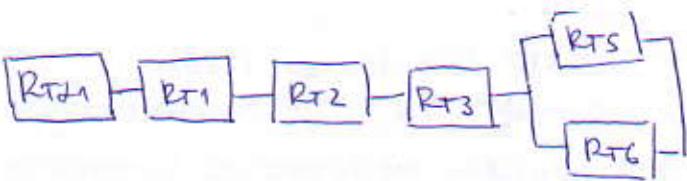


⇒ Šema otpornika:

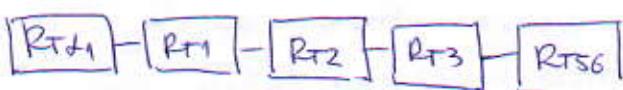


$$R_{T5} = R_{T45} + R_{T55} + R_{T+25}$$

$$R_{T6} = R_{T46} + R_{T66} + R_{T+26}$$



$$\frac{1}{R_{TS6}} = \frac{1}{R_{TS}} + \frac{1}{R_{TG}} \Rightarrow R_{TS6} = \frac{R_{TS} \cdot R_{TG}}{R_{TS} + R_{TG}}$$



$$R_T = R_{T1} + R_{T2} + R_{T3} + R_{TS6}$$

- ukupna površina zida: $S = S_1 \cdot 2,7 = 13,5 \text{ m}^2$

- površina zida sa malterom: $S_5 = 1,5 \cdot 2,7 = 4,05 \text{ m}^2$

- površina zida sa gipsom: $S_6 = 3,5 \cdot 2,7 = 9,45 \text{ m}^2$

$$R_{T1} = \frac{1}{d_1 \cdot S} = 0,0125976 \frac{\text{K}}{\text{W}}$$

$$R_{T1} = \frac{d_1}{\lambda_1 \cdot S} = 5,787 \cdot 10^{-4} \frac{\text{K}}{\text{W}}$$

$$R_{T2} = \frac{d_2}{\lambda_2 \cdot S} = 1,587 \cdot 10^{-3} \frac{\text{K}}{\text{W}}$$

$$R_{T3} = \frac{d_3}{\lambda_3 \cdot S} = 0,01214 \frac{\text{K}}{\text{W}}$$

$$R_{TS5} = \frac{d_4}{\lambda_4 \cdot S_5} = 0,21164 \frac{\text{K}}{\text{W}}$$

$$R_{TS6} = \frac{d_4}{\lambda_4 \cdot S_6} = 0,0907 \frac{\text{K}}{\text{W}}$$

$$R_{TS5} = \frac{d_5}{\lambda_5 \cdot S_5} = 3,52 \cdot 10^{-3} \frac{\text{K}}{\text{W}}$$

$$R_{TG6} = \frac{d_6}{\lambda_6 \cdot S_6} = 3,0234 \cdot 10^{-3} \frac{\text{K}}{\text{W}}$$

$$R_{T25} = \frac{1}{d_2 \cdot S_5} = 0,04199 \frac{\text{K}}{\text{W}}$$

$$R_{T26} = \frac{1}{d_2 \cdot S_6} = 0,017997 \frac{\text{K}}{\text{W}}$$

$$R_{TS} = R_{TS5} + R_{TS5} + R_{T25} = 0,25715 \frac{\text{K}}{\text{W}}$$

$$R_{TG} = R_{TG6} + R_{TG6} + R_{T26} = 0,1192 \frac{\text{K}}{\text{W}}$$

$$R_{TS6} = \frac{R_{TS} \cdot R_{TG}}{R_{TS} + R_{TG}} = 0,076743 \frac{\text{K}}{\text{W}}$$

$$R_T = R_{T1} + R_{T2} + R_{T3} + R_{TS6} = 0,10364 \frac{\text{K}}{\text{W}}$$

\rightarrow R-vrednost zida: $R = R_T \cdot S$

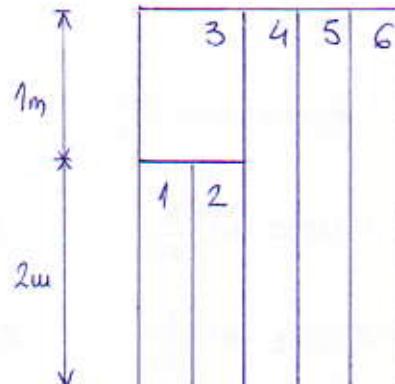
$$R_S = R_{TS} \cdot S_5 = 1,04015 \frac{\text{K} \cdot \text{m}^2}{\text{W}} \quad R_6 = R_{TG} \cdot S_6 = 1,10754 \frac{\text{K} \cdot \text{m}^2}{\text{W}}$$

$$R_{S6} = \frac{R_S \cdot R_6}{R_S + R_6} = 0,5364 \frac{\text{K} \cdot \text{m}^2}{\text{W}}$$

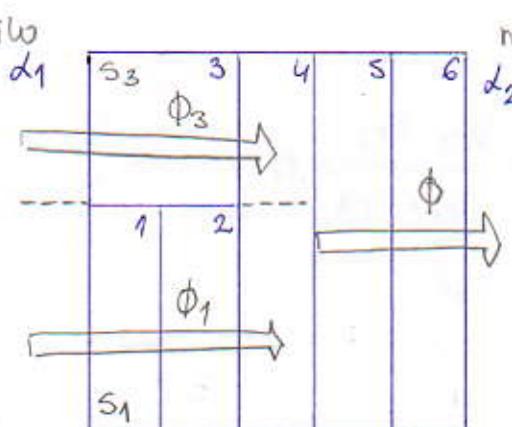
$$R = (R_{T1} + R_{T2} + R_{T3} + R_{TS6}) \cdot S + R_{S6} = 0,89994 \frac{\text{K} \cdot \text{m}^2}{\text{W}}$$

3) Izračunati ekvivalentni termički otpor za prolaz toplote i R vrednost zida za ravan višeslojni zid dužine 3m i visine 3,5m čije su dimenzije i poprečni presek prikazani na slici. Zid razdvaja kapatilo od negrejanog hodnika i deo je termičkog omotača zgrade. Koeficijenti prelaza toplote sa spoljašnje i unutrašnje strane zida su jednaki i iznose $7,69 \frac{W}{K \cdot m^2}$. Koeficijenti toplotne provodnosti za pojedine materijale su dati u tabeli. Prvi sloj u tabeli se nalazi sa unutrašnje strane zida, a poslednji sa spoljašnje.

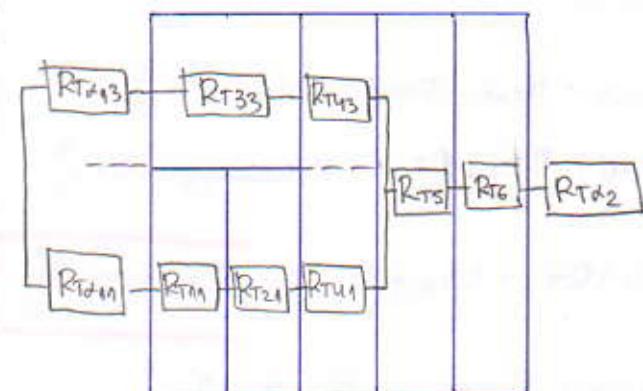
Br.	Materijal	Deklijina d [cm]	$\lambda \left[\frac{W}{m \cdot K} \right]$
1	Keramičke pločice	1	1,28
2	Cementni estrih	1,5	1,4
3	Krečnogipsani malter	2,5	0,7
4	Armirani beton	12	2,33
5	Kamena vuna	4	0,04
6	Malter	1	1,4



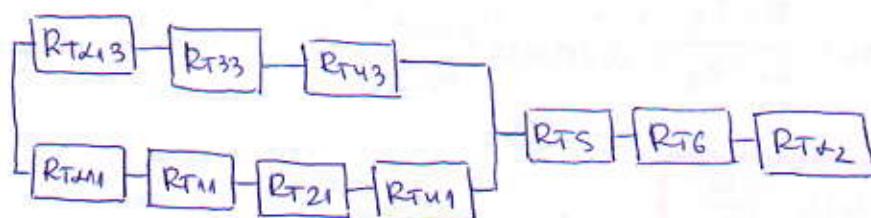
kapatilo



negrejani
hodnik

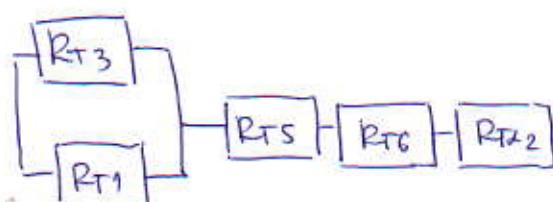


→ Šema otpornika:

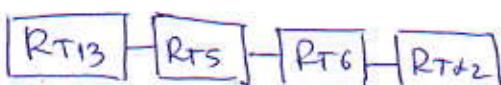


$$RT_3 = RT_{13} + RT_{33} + RT_{43}$$

$$RT_1 = RT_{11} + RT_M + RT_{21} + RT_{U1}$$



$$\frac{1}{RT_{13}} = \frac{1}{RT_1} + \frac{1}{RT_3} \Rightarrow RT_{13} = \frac{RT_1 \cdot RT_3}{RT_1 + RT_3}$$



$$R_T = RT_{13} + RT_5 + RT_6 + RT_{2+}$$

→ ukupna povrsina zida: $S = 3 \cdot 3,5 = 10,5 \text{ m}^2$

→ povrsina zida sa malterom: $S_3 = 1 \cdot 3,5 = 3,5 \text{ m}^2$

→ povrsina zida sa keramickim pločicama: $S_1 = 2 \cdot 3,5 = 7 \text{ m}^2$

$$RT_{d2} = \frac{1}{\lambda_2 \cdot S} = 0,012385 \frac{\text{K}}{\text{W}} \quad RT_6 = \frac{d_6}{\lambda_6 \cdot S} = 6,8027 \cdot 10^{-4} \frac{\text{K}}{\text{W}}$$

$$RT_5 = \frac{d_5}{\lambda_5 \cdot S} = 0,09524 \frac{\text{K}}{\text{W}}$$

$$RT_{d11} = \frac{1}{\lambda_1 \cdot S_1} = 0,0185774 \frac{\text{K}}{\text{W}} \quad RT_{d13} = \frac{1}{\lambda_1 \cdot S_3} = 0,037154 \frac{\text{K}}{\text{W}}$$

$$RT_M = \frac{d_1}{\lambda_1 \cdot S_1} = 1,11607 \cdot 10^{-3} \frac{\text{K}}{\text{W}} \quad RT_{33} = \frac{d_3}{\lambda_3 \cdot S_3} = 0,0102 \frac{\text{K}}{\text{W}}$$

$$RT_{21} = \frac{d_2}{\lambda_2 \cdot S_1} = 1,5306 \cdot 10^{-3} \frac{\text{K}}{\text{W}} \quad RT_{43} = \frac{d_4}{\lambda_4 \cdot S_3} = 0,0147 \frac{\text{K}}{\text{W}}$$

$$RT_{M1} = \frac{d_4}{\lambda_4 \cdot S_1} = 7,3574 \cdot 10^{-3} \frac{\text{K}}{\text{W}}$$

$$RT_3 = RT_{d13} + RT_{33} + RT_{43} = 0,06205 \frac{\text{K}}{\text{W}} \quad RT_1 = RT_{d11} + RT_M + RT_{21} + RT_{M1} = 0,02858 \frac{\text{K}}{\text{W}} \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} RT_{13} = \frac{RT_1 \cdot RT_3}{RT_1 + RT_3} = 0,019567 \frac{\text{K}}{\text{W}}$$

$$RT = RT_{13} + RT_5 + RT_6 + RT_{d2} = 0,12787 \frac{\text{K}}{\text{W}}$$

-R-vrednost zida $R = RT \cdot S$

$$R_3 = RT_3 \cdot S_3 = 0,217175 \frac{\text{K} \cdot \text{m}^2}{\text{W}} \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} R_{13} = \frac{R_1 \cdot R_3}{R_1 + R_3} = 0,10413 \frac{\text{K} \cdot \text{m}^2}{\text{W}}$$
$$R_1 = RT_1 \cdot S_1 = 0,20006 \frac{\text{K} \cdot \text{m}^2}{\text{W}}$$

$$R = R_{13} + (RT_5 + RT_6 + RT_{d2}) \cdot S = 1,2413 \frac{\text{K} \cdot \text{m}^2}{\text{W}}$$

saradnik Milica Radojičić